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# Power Plant Engineering-1

Classroom Notes

[Handwritten]

FOR GATE I ESE I PSU'S

**Mechanical Engineering** 

By: Mr. Praveen Kulkarni

# Index

- 1. Vapour power cycles
- 2. Gas turbines
- 3. Air compressors

### Vapour power Cycles

Reason's for using water as working fluid-

- It is cheap.

-> It is chemically stable.

7th = 35-424, pressure natio = 180 to 300 )

Max temp- 620'c

weight/power=55kg/

SPP.

> It is nontoxic.

## Selection of a power plant-

Efforts to improve efficiency and thereby reducing the running cost or operating cost may be desirable and this would lead to increase initial or capital powe cost, and hence efforts must be taken to optimise the total cost.

# Specific Steam Consumption (SSC):

$$SSC = \frac{\dot{m}_{S}}{P_{net}} = \frac{\dot{m}_{S}}{\dot{m}_{S} \times W_{net}}$$

$$SSC = \frac{1}{W_{net}} \frac{kg}{kJ} | W_{net} \rightarrow \frac{kJ}{kg}.$$

$$SSC = \frac{1}{W_{net}} \frac{kg}{kJ_{XSec}} \Rightarrow \frac{1}{W_{net}} \frac{kg}{kw_{Sec}}$$

$$SSC = \frac{3600}{W_{net}} \frac{kg}{kw_{hr}} \left\{ \frac{W_{net}}{W_{net}} \right\} \frac{1}{Sec} = \frac{1}{3600} \frac{kg}{3600}$$

Significance of SSC: ssc indicates size of the plant smaller the ssc larger is the net work and hence for developing given power. mass Flow rate of steam must be less that is smaller the SSC, & lesson is the size of the plant and hence Such plants ane preferable.

Work Ratio:-It is the ratio of Net work to the tve work.

$$\gamma_{w} = \frac{Wnet}{+ve\ Work}$$

$$\Rightarrow \frac{W_{+ve} - W_{-ve}}{W_{+ve}}$$

$$Y_W = 1 - \frac{W_{-Ve}}{W_{+Ve}}$$

$$Y_{W} = 1 - \frac{Wp}{WT}$$

pump - liquid

compressor- gas

pump work is less

- power plants with high work ratio's are preferable.
- → Work ratio is highest for rankine cycle, among all other cycles
  this is because in rankine cycle, work is used which consumes
  pump
- → In case of gas twibine power plant the work ratio is about 0.4 to 0.6 i.e. in gas twibine power plant compressor about 40 60% Of twibine work.
- In rankine cycle the work ratio are about 0.96-0.98 (
  close to unity) i.e. in rankine cycle pump consumes 2-4% of
  twobine work.

Back work Ratio ( Tow): It is the ratio of -ve work to the +ve work.

$$\gamma_{bw} = \frac{W-ve}{W+ve}$$

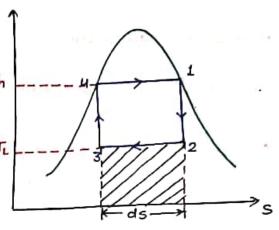
$$Y_W = \frac{W_{\text{Net}}}{W_{\text{tve}}} = \frac{W_{\text{tve}} - W_{\text{-ve}}}{W_{\text{tve}}} \Rightarrow 1 - \frac{W_{\text{-ve}}}{W_{\text{tve}}} = 1 - Y_{\text{bW}}$$

$$\gamma_W = 1 - \gamma_{bW}$$



(1) Saturated vapour which is entering the turbine at 1 leaves at 2 which is in wet region. The liquid which is present at state 2 may damage turbine blades due to high velocity.

Carnot Vapour power Cycle:



(2) It is difficult to design a condenser which suddenly stops at point 3. (3) It is difficult to design a compressor which handles both

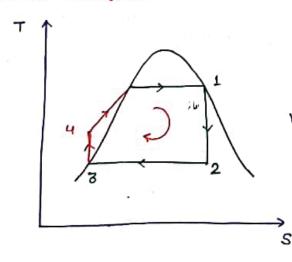
liquid and vapows.

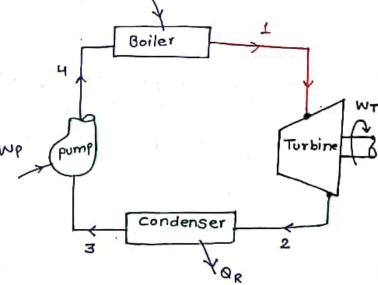
(4) As council vapour power cycle usages compressor, the compressor work is large and hence Net work is less. [What = WT-Wc]

$$\eta = 1 - \frac{Q_R}{Q_S}$$
  $\Rightarrow$   $1 - \frac{T_L ds}{T_H ds}$ 

$$\eta = 1 - \frac{T_L}{T_h}$$

#### Rankine Cycle:-





Qs

$$\eta = \frac{W_{\text{net}}}{Q_s}$$

$$\eta = \frac{W_T - W_P}{Q_S}$$

1-2 - Reversible adiabatic Expansion (Turbine)

2-3 → constant pressure heat Rejection (condenser)

3-4 → Rev. adiabatic compression ( pump)

4-1 - constant pressure heat addition (boiler)

#### Analysis of the cycle :-

Assumptions:

treated

(1) Each device is Fitted at steady Flow device.

, (2) K.E & P.E. changes are Neglected.

(3)

Twibine (1-2) [ Reversible adiabatic]

$$h_1 + \frac{c_1 z}{z} + z_1 g + g = h_2 + \frac{c_2 e}{z} + z_2 g + w$$

$$h_1 = h_2 + w$$

$$W_{\text{Turbine}} = h_1 - h_2$$

Condenser (2-3)

$$h_1 + \frac{c_2^4}{2} + \frac{z_2}{9} + 9 = h_3 + \frac{c_3^3}{2} + \frac{z_3}{2} + \frac{z_3}{9} + \psi$$
 (No work)

$$-9 = h_2 - h_3.$$

$$\Rightarrow 9 \text{ rejection} = h_2 - h_3$$

pump (3-4):

-ve represent work done on the System.

Boller (4 1) 40 + CA Note: - We know that open system work W= - vdp this equation is applicable when the Flow is steady, KE f PE changes are Neglected and when the process is reversible. SFEE can be applied for rev. as well as irreversible process If the pumping process is reversible then work obtained for SFEE and w= -vdp can be equated.  $h_3 - h_0 = -VdP$ hu-h3 = Vdp 7 → We know that Wp = hu-hz, if the pump work is Very small then it can be neglected therefore hu - ha when pump work is Negligible. Boiler:-[4-1] hu+ 5/2 + z/9 + 9 = h,+ 5/2 + z/9 + W [No work] 9  $h_4 + 2 = h_1$ 9 = h,-h4 ; 9 = h,-h4 W- = h1-h2  $\eta = \frac{W_T - W_P}{Q_C}$ 7 Q = h2-h3 )  $\eta = \frac{(h_{43} - h_2) - (h_4 - h_3)}{(h_1 - h_4)}$ Wp= hu-ha 95 = h1-h4 when pump work is Ngligible hu= h3  $\Rightarrow \qquad \boxed{ \eta = \frac{h_1 - h_2}{h_1 - h_3} }$  $\eta = \frac{h_1 - h_2}{h_1 - h_2}$