

Hindbookcenter



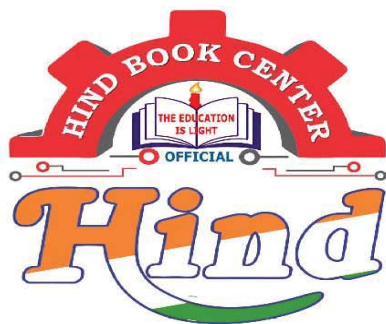
Hind Book Center & Photostat

MADE EASY **Civil Engineering** **Toppers Handwritten Notes** **DESIGN OF STEEL STRUCTURES** **By-Vijay Pahwa Sir**

- Colour Print Out
- Blackinwhite Print Out
- Spiral Binding,& Hard Binding
- Test Paper For IES GATE PSUs IAS, CAT, SSC
- All Notes Available & All Book Availabie
- Best Quaity Handwritten Classroom Notes & Study Materials
- IES GATE PSUs IAS SSC Other Competitive/Entrence Exams

Visit us:-www.hindbookcenter.com

Courier Facility All Over India
(DTDC & INDIA POST)
Mob-9654353111



Hindbookcenter



ALL NOTES BOOKS AVAILABLE ALL STUDY MATERIAL AVAILABLE

COURIERS SERVICE AVAILABLE

MADE EASY, IES MASTER, ACE ACADEMY, KREATRYX

ESE, GATE, PSUs BEST QUALITY TOPPER HAND WRITTEN NOTES

MINIMUM PRICE AVAILABLE @ OUR WEBSITE

- | | |
|--------------------------------|---------------------------|
| 1. ELECTRONICS ENGINEERING | 2. ELECTRICAL ENGINEERING |
| 3. MECHANICAL ENGINEERING | 4. CIVIL ENGINEERING |
| 5. INSTRUMENTATION ENGINEERING | 6. COMPUTER SCIENCE |

IES, GATE, PSU TEST SERIES AVAILABLE @ OUR WEBSITE

❖ IES –PRELIMS & MAINS

❖ GATE

➤ NOTE;- ALL ENGINEERING BRANCHS

➤ ALL PSUs PREVIOUS YEAR QUESTION PAPER @ OUR WEBSITE

PUBLICATIONS BOOKS -

MADE EASY, IES MASTER, ACE ACADEMY, KREATRYX, GATE ACADEMY, ARIHANT, GK

RAKESH YADAV, KD CAMPUS, FOUNDATION, MC –GRAW HILL (TMH), PEARSON...OTHERS

HEAVY DISCOUNTS BOOKS AVAILABLE @ OUR WEBSITE

Shop No.7/8 Saidulajab Market Neb Sarai More, Saket, New Delhi-30 9654353111	Shop No: 46 100 Futa M.G. Rd Near Made Easy Ghitorni, New Delhi-30		
--	---	--	--

Website: www.hindbookcenter.com

Contact Us: 9654353111

Design of Steel Structure

GATE :- $2M - 1Q = 2M$
 $2Q - 1M = 2M \rightarrow 4M$

ESE: (Pre) :- 10 - 15Q (20-30M)

(Mains) :- 60M

BARC }
ISRO } 10% Q
DRDO } Steel

[S.K Duggal]

IS 800:2007 [L.S.M]

800:1984 (WSM)

Steel Table

Syllabus

2] Design Philosophy (ESE)

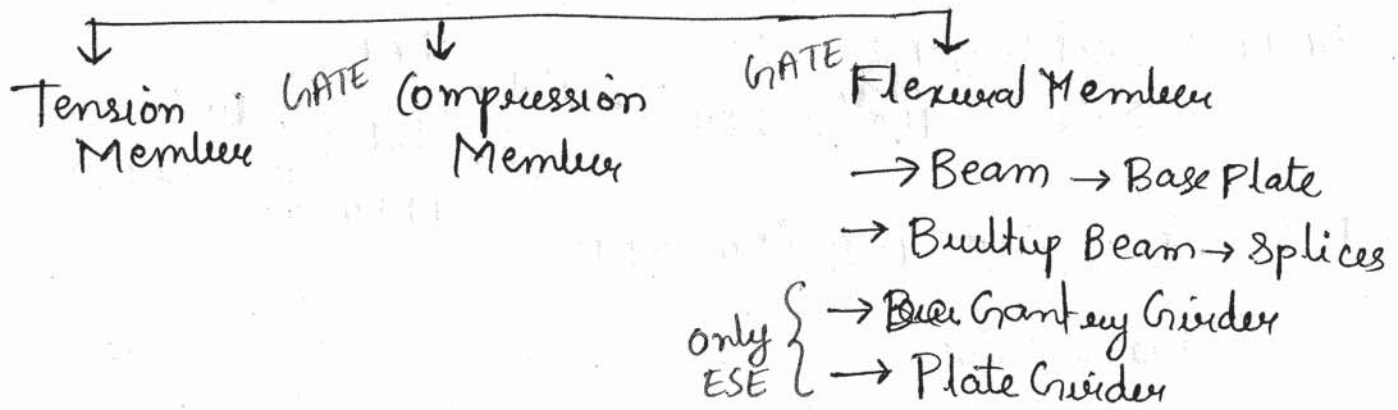
- WSM
- Plastic Method of design
- Limit State method of Design

3] Connection Design

Simple Connection (GATE) Eccentric

- Rivets
 - Bolts
 - Welding
- GATE/ESE
- Type I
 - Type II

4] Member Design (ESE)



6] Industrial Roof (ESE)

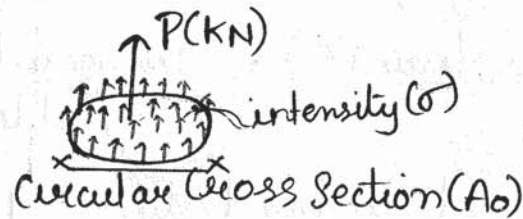
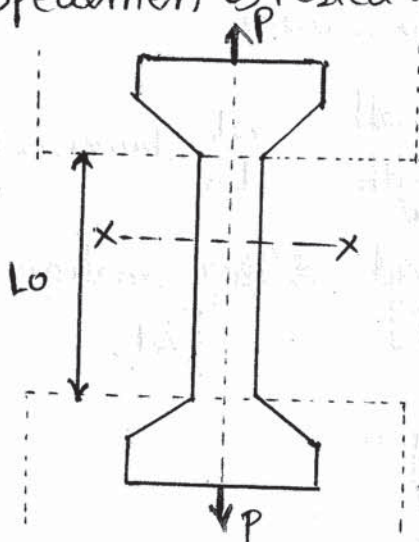
- Roof truss
- Purlin

Chapter 1: Plastic Analysis of Beams & Frame

Stress Strain Curve for Mild Steel

→ A tensile test is conducted on a Mild steel specimen (ie coupon)

→ Specimen is tested in universal testing machine (U.T.M)

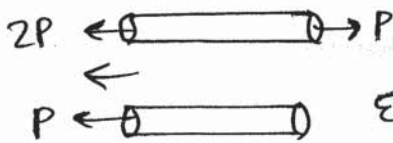


$A_0 \rightarrow$ Original cross sectional area (mm^2)

$P \rightarrow$ Applied load (KN)

$\sigma \rightarrow$ Nominal Tensile stress

$$\sigma = P/A_0$$



$\epsilon F = 0$ { Rigid body Translation }

→ As material is assumed to be homogenous & Isotropic, the intensity distribution of load on the cross section can be assumed to be equal

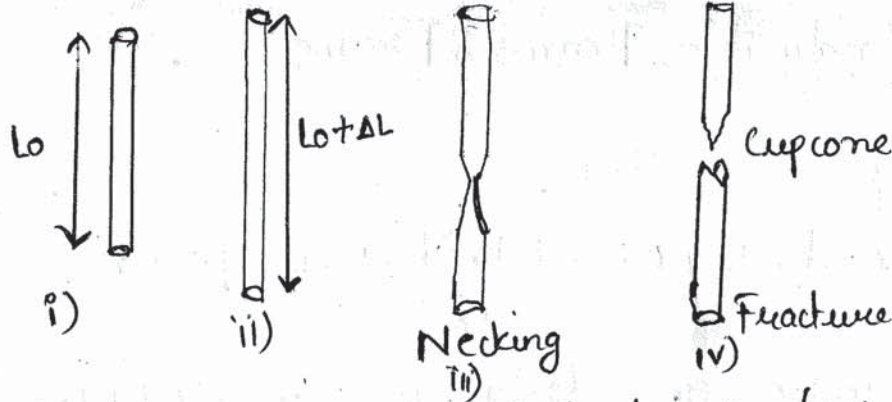
→ The intensity of load over cross-sectional is termed as stress

$$\left[\sigma = \frac{P}{A_0} \frac{(\text{N})}{(\text{mm}^2)} \rightarrow \text{Unit N/mm}^2 \text{ or MPa} \right]$$

→ The length over which specimen is tested is called as gauge length & it is given by

$$L_0 = 5.65 \sqrt{A_0}$$

→ Specimen is subjected to gradually increasing tensile loading

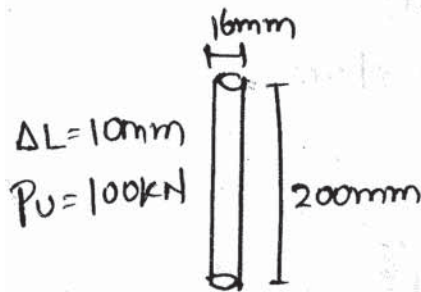


ΔL = change in length (mm) / Extension / Deformation

→ Normal tensile strain (ϵ) $\Rightarrow \frac{\text{change in length}}{\text{original length}} = \frac{\Delta L}{L_0}$ (Dimensionless)

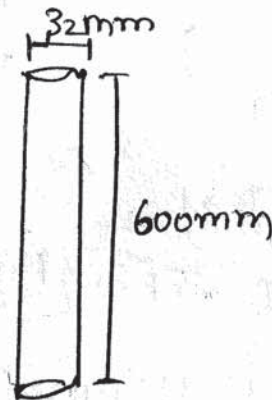
→ Reading observed during testing → Load [P] & Deformation [ΔL]

Always (same) Stress
Strain



$$\sigma_u = \frac{P_u}{A_0} = \frac{100 \times 10^3}{\frac{\pi}{4} \times 16^2} = 497.36 \text{ N/m}^2$$

$$\epsilon = \frac{\Delta L}{L} = \frac{10}{200} = 5 \times 10^{-2}$$



$$\sigma_u = \frac{P_u}{A_0} \therefore 497.36 = \frac{P_u}{\frac{\pi}{4} \times 32^2}$$

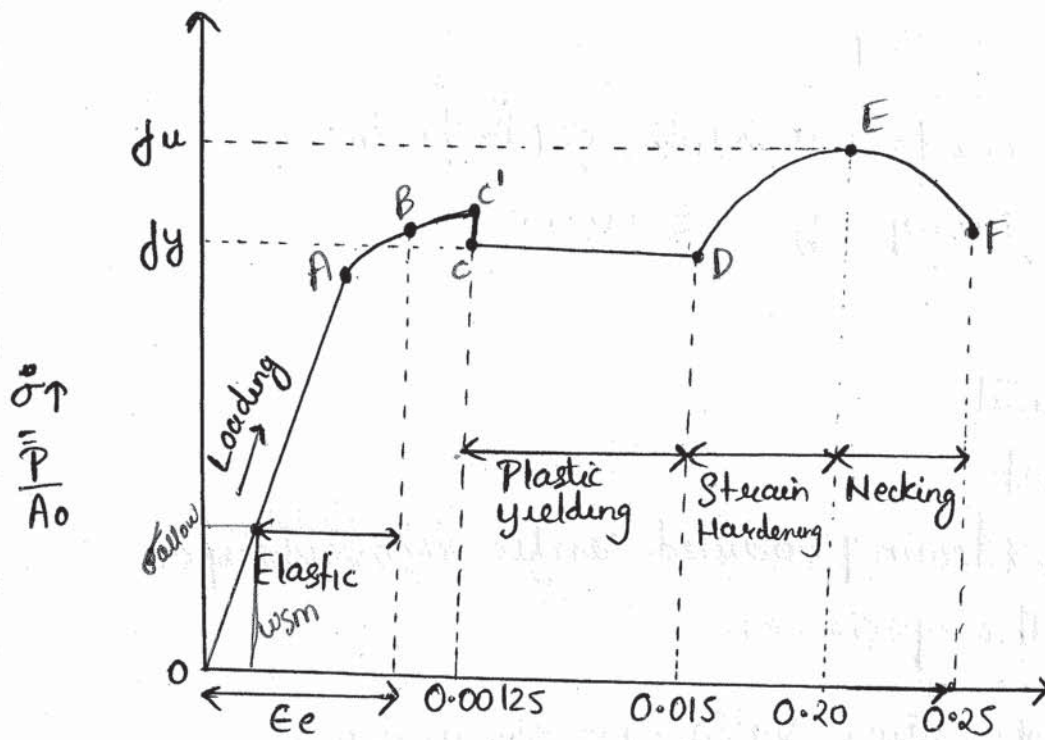
$$P_u = \underline{400 \text{ kN}}$$

$$\epsilon = 5 \times 10^{-2} = \frac{\Delta L}{600}$$

$$\Delta L = 30 \text{ mm}$$

→ P- Δ graph will be different for different size of specimen

→ Hence σ - ϵ curve is plotted for specimen { It will be same for a given material }



$$\frac{\Delta L}{L_0} = \epsilon \rightarrow$$

d_y = yield strength (N/mm^2)

d_u = Ultimate tensile strength (N/mm^2)

(y)	(x)	Slope = $\frac{dy}{dx} = \frac{y_2 - y_1}{x_2 - x_1}$	} ex. for graph
P	ΔL		
0	0		
i) 10kN	1mm	$\frac{20-10}{2-1} = 10 \text{ kN/mm}$	
ii) 20kN	2mm	$\frac{30-20}{3-2} = 10 \text{ kN/mm}$	
iii) 30kN	3mm	$\frac{38-30}{4-3} = 8 \text{ kN/m}$	
iv) 38kN	4mm		

$$y = m \cdot x$$

$y \propto x$

\Rightarrow Imp Points :-

i] Region OA

\rightarrow A is a proportional limit

\rightarrow Graph is linear (ie slope is constant)

→ $\sigma \propto E$ (Hook's law)

→ $\sigma = E \cdot \epsilon$, $\frac{\sigma}{\epsilon} = E$

→ E = Elastic constant / Modulus of Elasticity

$E = \tan \theta \rightarrow$ Slope of σ, ϵ curve

2] Region AB

→ B → Elastic limit

→ Linearity is lost

→ upto point B, strain produced can be recovered upon unloading of the specimen

→ Assume: Hook's law is Valid upto elastic limit

3] Region B - C' - C

→ C' = upper yield point {transient → short interval}

→ C = Lower yield point {stable, designates yield strength of material}

→ It is a point below which material behaves elastically

Above which material behaves plastically

4] C - D Region

→ Plastic yielding or yield Plateau

→ Material/specimen deforms to very large extent without resisting any stress

→ It is a limiting slope

→ Fielding Failure

5] Region D-E

- Strain Hardening
- Specimen re-crystallizes due to which it resists stresses along with its further extension
- It occurs upto point E
- E \Rightarrow Point of Ultimate strength
- Till Date this part is not usedⁱⁿ design

6] E-F Region

\Rightarrow ~~Necking~~ \Rightarrow

- Necking: Reduction in cross sectional area
- F \Rightarrow Breaking point / Fracture point
- Fracture is also termed as Rupture
- Shape: Cup & Cone failure

\Rightarrow Mechanical property from σ & ϵ curve

1) σ_y

3) E

2) σ_u

4) Ductility

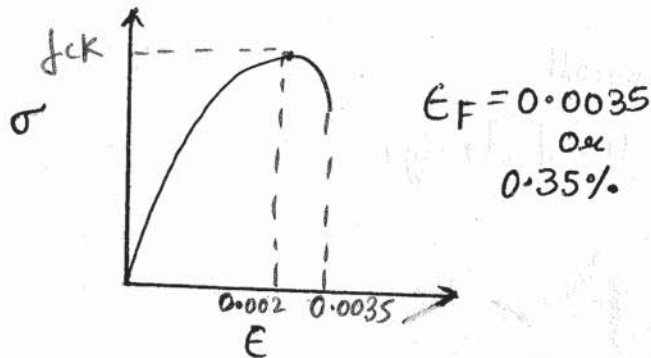
\Rightarrow Ductility: Ability of material to undergo large deformation without breaking. It is measured in terms of % Elongation

$$\% \text{ elongation} = \frac{\text{Final length} - \text{Gauge length}}{\text{Gauge length}} \times 100$$

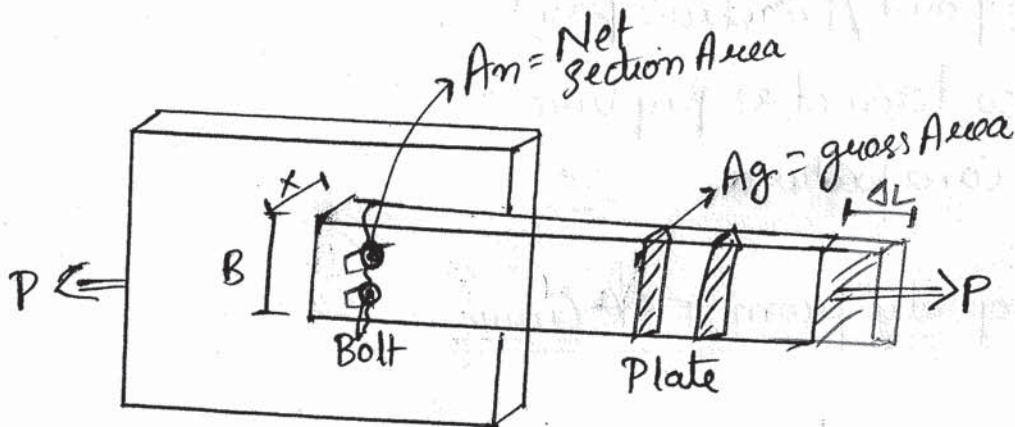
% Elongation	Material
> 15%	Ductile (Steel, Al)
15 - 5%	Interm. Ductile (Mn)
< 5%	Brittle (concrete, cast iron)

→ Toughness:- Resistance to impact loading

Concrete Compression test

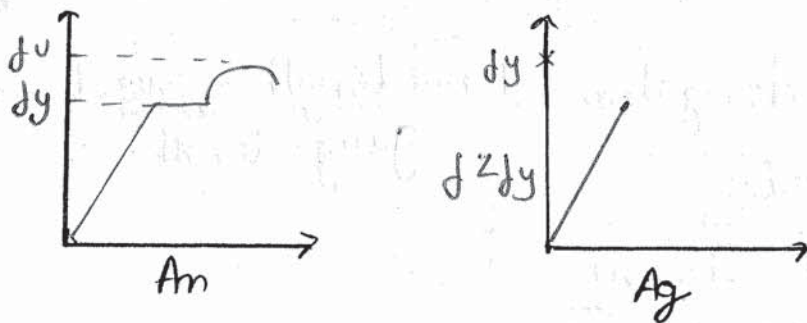


⇒ Practical Case of Tension member



There are two type of limiting stage

- 1) Gross Section yielding
- 2) Net-Section Rupture

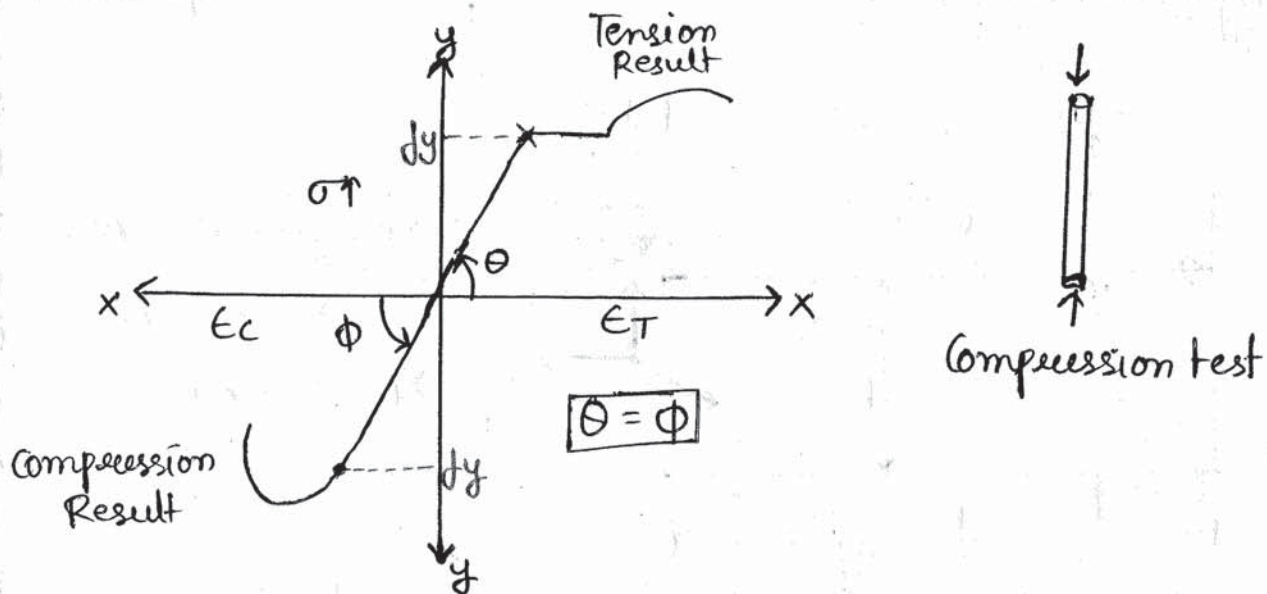


Note:

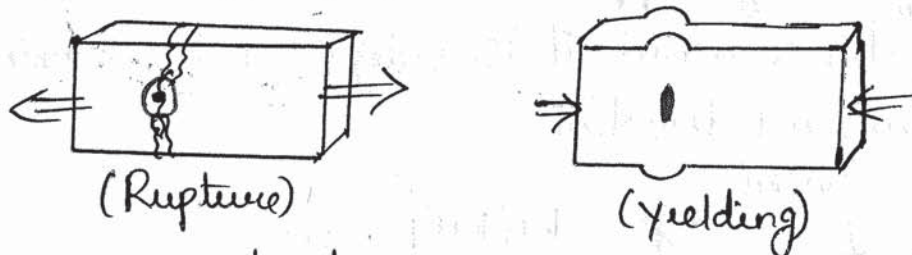
→ For design of tension member connected with Rivet/Bolts there are two types of limit state

- 1) Gross section yielding 2) Net section Rupture

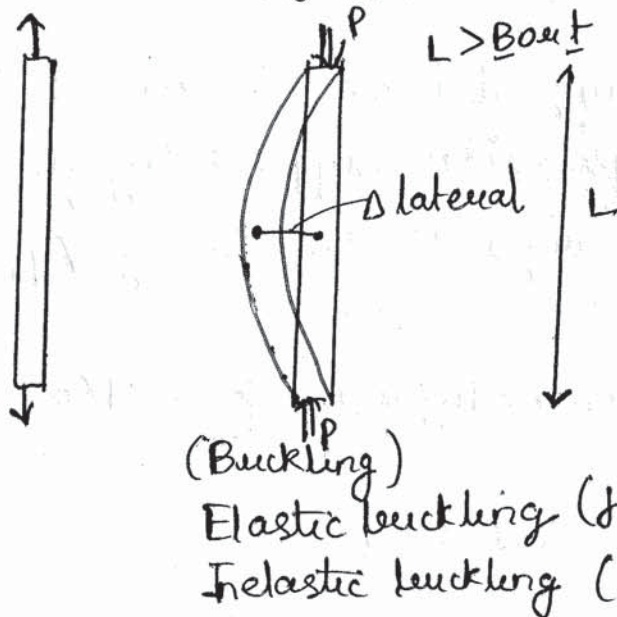
Compressive σ - ϵ Curve for mild steel



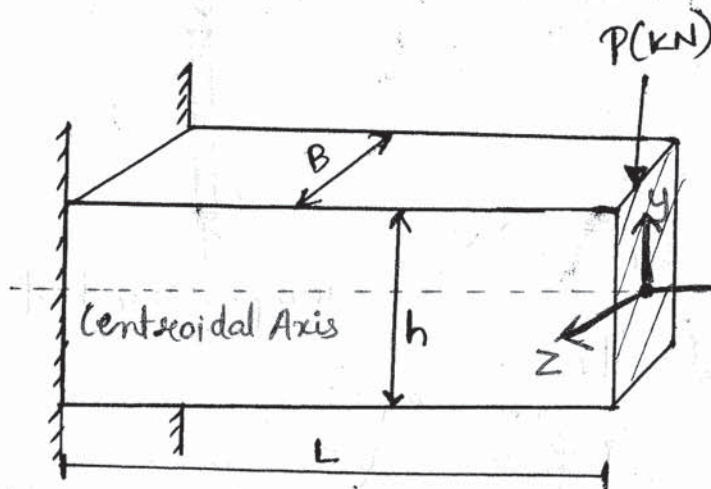
- Steel is equally strong in tension as well as in compression
- Modulus of Elasticity in tension = Modulus of elasticity in compression



- Type of limit stage for compression member
 - 1) Gross section yielding (f_y)
 - 2) Lateral buckling ($f < f_y$)



Bending and shear Stress



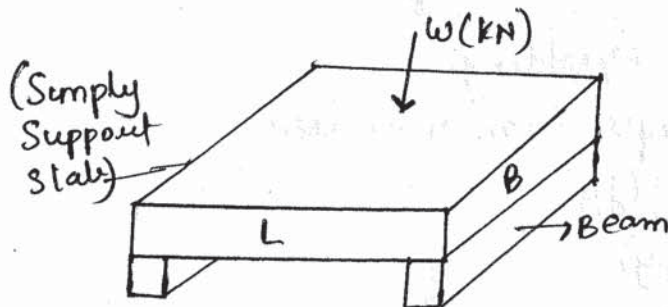
X → longitudinal Axis

Y → Transverse Axis

Z → Lateral Axis

→ Flexural Member such as beam are subjected to transverse loading due to which internal Forces/Moment Produced are shear force & Bending moment

→ Load :- Beam generally support slabs or other beam over it, due to which it is subjected to loading in downward direction



$$\frac{W(kN)}{B \times L(m^2)} = w$$

→ Reaction :- Beam are supported over columns or other beam which provides support by generating Forces/Moment in opposite direction of Applied loading / Moment

Notes Reactions are determine by using force Moment Equilibrium

$$\{\sum F = 0, \sum M = 0\}$$

→ Types of Support :-



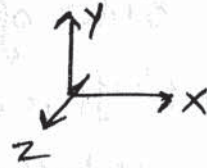
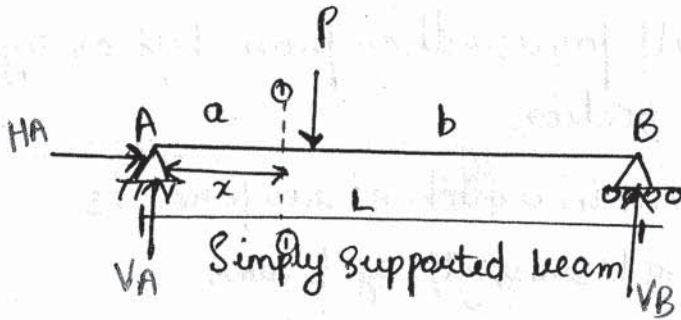
Roller support ; →



Hinge Support ;



Fixed Support



$$\sum F_x = 0 \rightarrow H_A = 0$$

$$\sum F_y = 0 \rightarrow V_A + V_B = P$$

$$\sum M_B = 0$$

Moment → Rotational effect of ^{external} Forces

$M = F \times \perp$ distance upto point

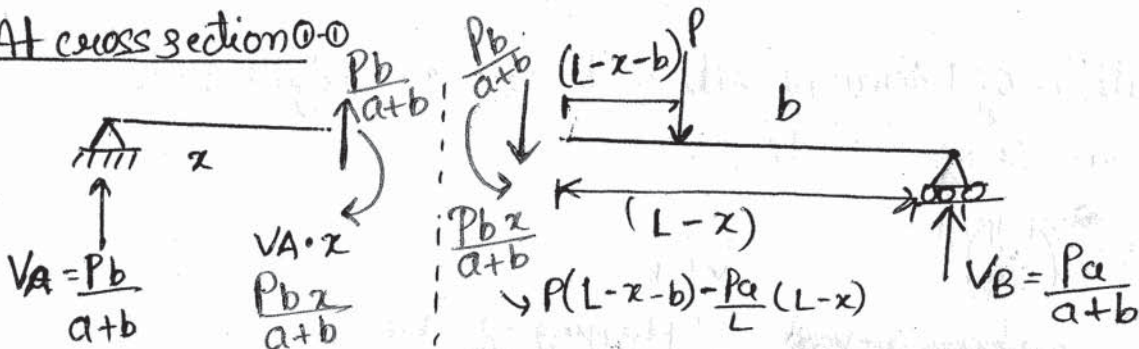
$$+ V_A \times L - P \times b = 0$$

$$V_A = \frac{Pb}{L} = \frac{Pb}{a+b}$$

Also, $V_B = P - V_A = P - \frac{Pb}{a+b}$

$$V_B = \frac{Pa}{a+b}$$

At cross section 0-0



→ At any cross section, let us take at a distance x from Support A $\{0 \leq x \leq a\}$

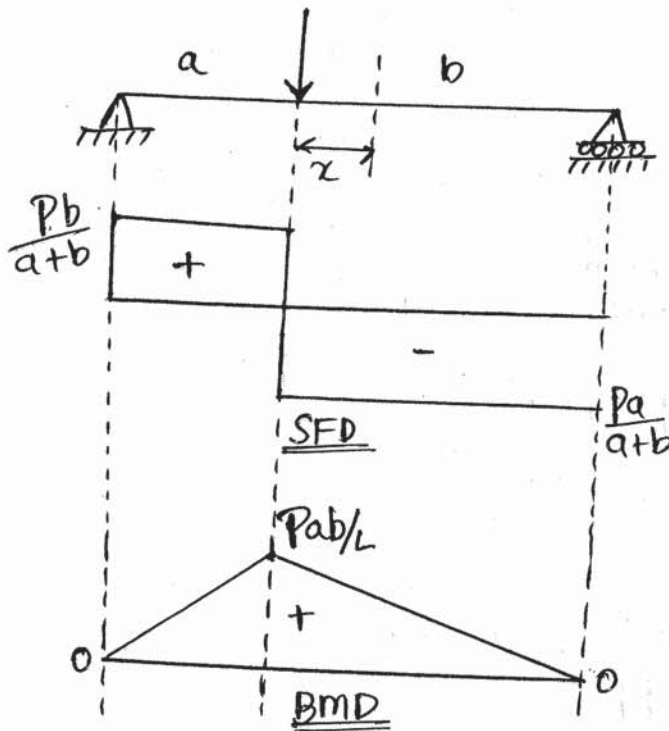
→ Resultant force in transverse direction $= \frac{Pb}{a+b}$

→ This ~~cat~~ is called as transverse shear force

Notes:

Shear force :- Summation of all forces either from left or right sides of cross section

Shear force dia :- It is a diagram in which shear force is plotted along the length of beam

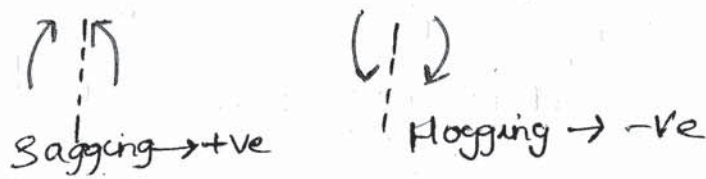


$$P - V_A = V_B = \frac{Pa}{a+b}$$

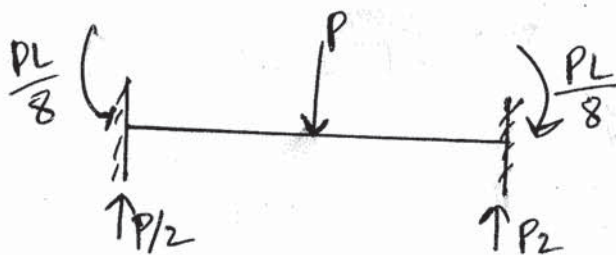
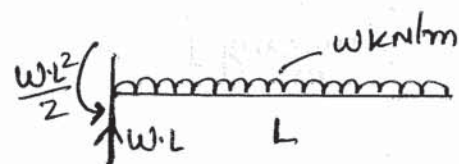
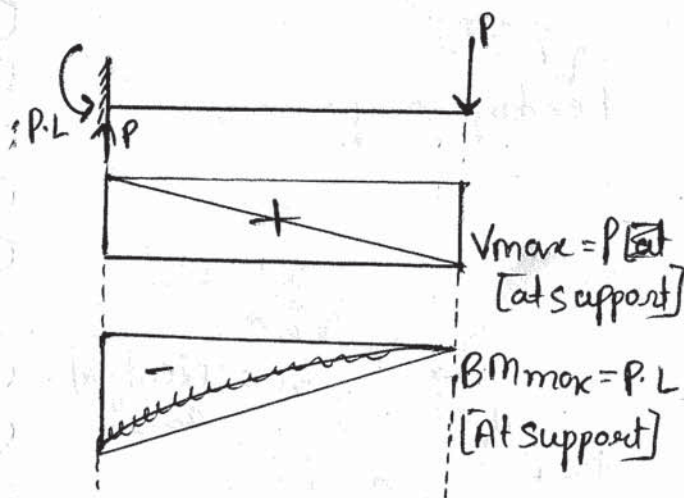
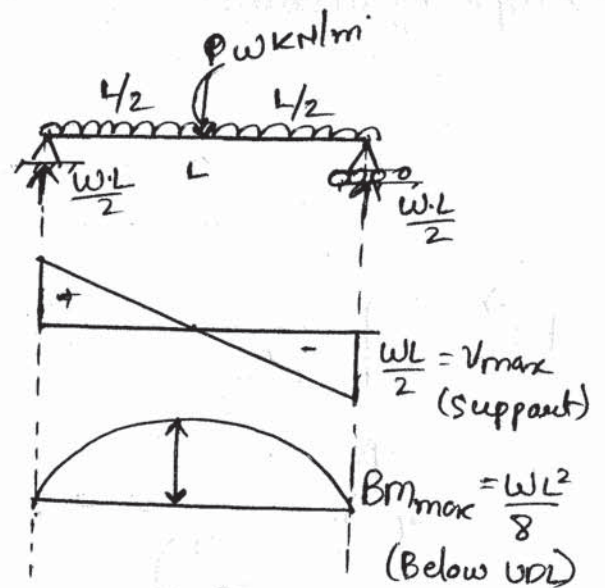
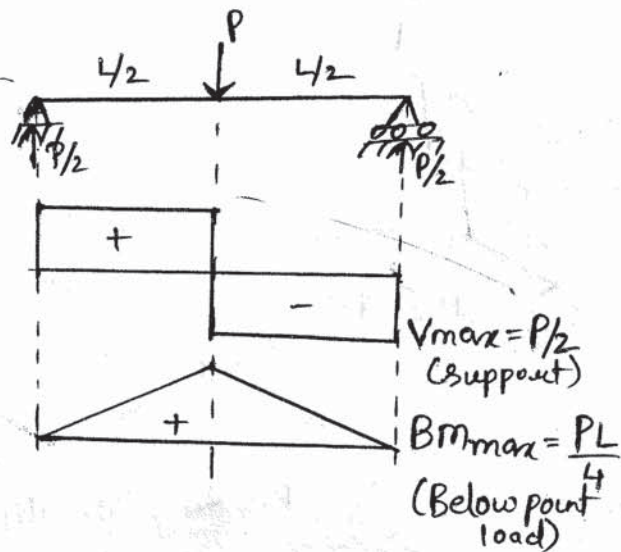
$$[0 \leq x \leq b]$$

Bending Moment :- It is the resultant Moment inside the Beam cross-section

→ Summation of Moment either to left or right side of Beam cross-section

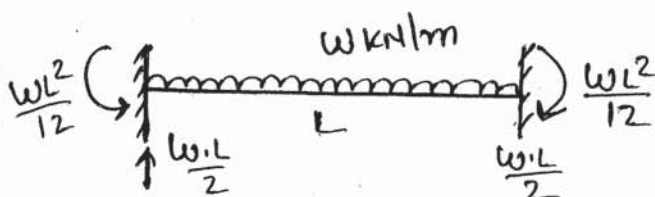


⇒ Standard Result



$$V_{\max} = \frac{P}{2}$$

$$B.M_{\max} = \frac{PL}{8}$$



$$V_{\max} = \frac{w.L}{2}$$
 (At support)
$$B.M_{\max} = \frac{w.L^2}{12}$$
 (At support)